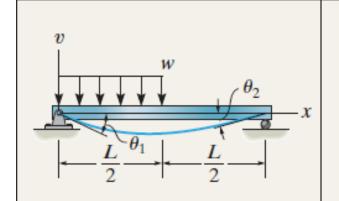
METHOD OF SUPERPOSITION

The differential equation $EI d^4v/dx^4 = w(x)$ satisfies the two necessary requirements for applying the principle of superposition; i.e., the load w(x) is linearly related to the deflection v(x), and the load is assumed not to change significantly the original geometry of the beam or shaft. As a result, the deflections for a series of separate loadings acting on a beam may be superimposed. For example, if v_1 is the deflection for one load and v_2 is the deflection for another load, the total deflection for both loads acting together is the algebraic sum $v_1 + v_2$. Using tabulated

Simply Supported Beam Slopes and Deflections

Simply Supported Beam Slopes and Deflections				
Beam	Slope	Deflection	Elastic Curve	
$\frac{v}{L}$ $\frac{L}{2}$ $\frac{L}{2}$ $\frac{L}{2}$	$\theta_{\text{max}} = \frac{-PL^2}{16EI}$	$v_{\text{max}} = \frac{-PL^3}{48EI}$	$v = \frac{-Px}{48EI}(3L^2 - 4x^2)$ $0 \le x \le L/2$	
e^{θ_1} e^{θ_2} e^{a} e^{b}	$\theta_{1} = \frac{-Pab(L+b)}{6EIL}$ $\theta_{2} = \frac{Pab(L+a)}{6EIL}$	$v\bigg _{x=a} = \frac{-Pba}{6EIL}(L^2 - b^2 - a^2)$	$v = \frac{-Pbx}{6EIL}(L^2 - b^2 - x^2)$ $0 \le x \le a$	
v θ_1 D M_0 X	$\theta_1 = \frac{-M_0 L}{6EI}$ $\theta_2 = \frac{M_0 L}{3EI}$	$v_{\text{max}} = \frac{-M_0 L^2}{\sqrt{243}EI}$ $\text{at } x = 0.5774L$	$v = \frac{-M_0 x}{6EIL} (L^2 - x^2)$	
v L w v d	$\theta_{\text{max}} = \frac{-wL^3}{24EI}$	$v_{\text{max}} = \frac{-5wL^4}{384EI}$	$v = \frac{-wx}{24EI}(x^3 - 2Lx^2 + L^3) $ Go to	



$$\theta_1 = \frac{-3wL^3}{128EI}$$

$$\theta_2 = \frac{7wL^3}{384EI}$$

$$v \bigg|_{x=L/2} = \frac{-5wL^4}{768EI}$$

$$v_{\text{max}} = -0.006563 \frac{wL^4}{EI}$$

at
$$x = 0.4598L$$

$$v \Big|_{x=L/2} = \frac{-5wL^4}{768EI} \qquad v = \frac{-wx}{384EI} (16x^3 - 24Lx^2 + 9L^3)$$
$$0 \le x \le L/2$$

$$v_{\text{max}} = -0.006563 \frac{wL^4}{EI}$$

$$v = \frac{-wL}{384EI} (8x^3 - 24Lx^2 + 17L^2x - L^3)$$

$$L/2 \le x < L$$

$$v$$
 θ_1
 L
 θ_2

$$\theta_1 = \frac{-7w_0L^3}{360EI}$$

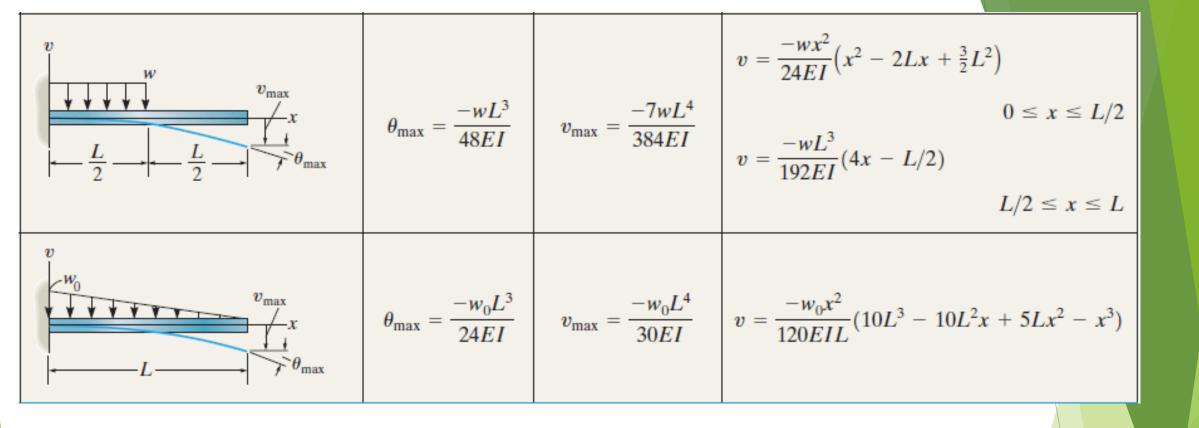
$$\theta_2 = \frac{w_0 L^3}{45EI}$$

$$v_{\text{max}} = -0.00652 \frac{w_0 L^4}{EI}$$

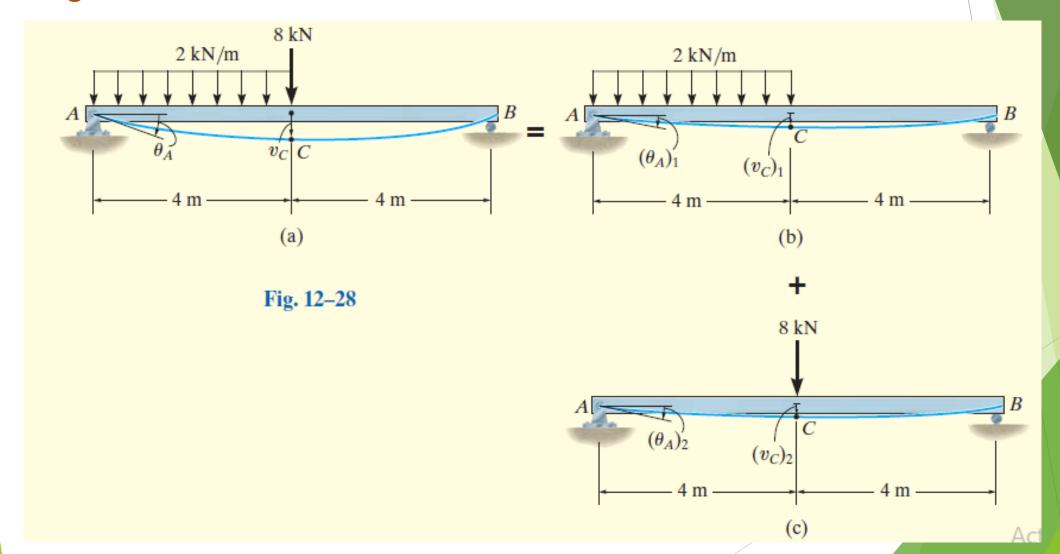
at
$$x = 0.5193L$$

$$v = \frac{-w_0 x}{360EIL} (3x^4 - 10L^2 x^2 + 7L^4)$$

Cantilevered Beam Slopes and Deflections					
Beam	Slope	Deflection	Elastic Curve		
v v_{max} θ_{max}	$\theta_{\text{max}} = \frac{-PL^2}{2EI}$	$v_{\text{max}} = \frac{-PL^3}{3EI}$	$v = \frac{-Px^2}{6EI}(3L - x)$		
v v v x d	$\theta_{\text{max}} = \frac{-PL^2}{8EI}$	$v_{\text{max}} = \frac{-5PL^3}{48EI}$	$v = \frac{-Px^2}{6EI} \left(\frac{3}{2}L - x\right) \qquad 0 \le x \le L/2$ $v = \frac{-PL^2}{24EI} \left(3x - \frac{1}{2}L\right) L/2 \le x \le L$		
v v v v d	$\theta_{\text{max}} = \frac{-wL^3}{6EI}$	$v_{\text{max}} = \frac{-wL^4}{8EI}$	$v = \frac{-wx^2}{24EI}(x^2 - 4Lx + 6L^2)$		
v θ_{max} M_0 v_{max}	$\theta_{\rm max} = \frac{M_0 L}{EI}$	$v_{\max} = \frac{M_0 L^2}{2EI}$	$v = \frac{M_0 x^2}{2EI}$ Actives Go to		



Example 1 Determine the displacement at point *C* and the slope at the support *A* of the beam shown in Figure. *El* is constant.



For the distributed loading,

$$(\theta_A)_1 = \frac{3wL^3}{128EI} = \frac{3(2 \text{ kN/m})(8 \text{ m})^3}{128EI} = \frac{24 \text{ kN} \cdot \text{m}^2}{EI} \downarrow$$
$$(v_C)_1 = \frac{5wL^4}{768EI} = \frac{5(2 \text{ kN/m})(8 \text{ m})^4}{768EI} = \frac{53.33 \text{ kN} \cdot \text{m}^3}{EI} \downarrow$$

For the 8-kN concentrated force,

$$(\theta_A)_2 = \frac{PL^2}{16EI} = \frac{8 \text{ kN}(8 \text{ m})^2}{16EI} = \frac{32 \text{ kN} \cdot \text{m}^2}{EI} \downarrow$$
$$(v_C)_2 = \frac{PL^3}{48EI} = \frac{8 \text{ kN}(8 \text{ m})^3}{48EI} = \frac{85.33 \text{ kN} \cdot \text{m}^3}{EI} \downarrow$$

The displacement at C and the slope at A are the algebraic sums of these components. Hence,

$$(+\downarrow) \qquad \qquad \theta_A = (\theta_A)_1 + (\theta_A)_2 = \frac{56 \text{ kN} \cdot \text{m}^2}{EI} \downarrow \qquad Ans.$$

$$(+\downarrow)$$
 $v_C = (v_C)_1 + (v_C)_2 = \frac{139 \text{ kN} \cdot \text{m}^3}{EI} \downarrow$ Ans.